A shallow water model forced by flow-dependent Ekman pumping Yanxu Chen¹, David Straub¹, Louis-Philippe Nadeau^{1,2}



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Ekman transport and pumping are known to be modified by surface currents.

	Ekman (1905)	Stern (1965)	Wenegrat & Thomas (2017)
Content	Transport depends on the stress and the Coriolis parameter only.	Allows for shear in the surface velocity field to affect the transport: "nonlinear" Ekman theory.	Extends Stern's results to better account for curvature in the surface flow path.
Ekman transport	$U_E = \frac{\tau_y}{f}$ $V_E = -\frac{\tau_x}{f}$	$U_E = \frac{\tau_y}{f + \zeta}$ $V_E = -\frac{\tau_x}{f + \zeta}$	$\begin{split} \varepsilon \bar{u} \frac{\partial V_E}{\partial s} + (1 + \varepsilon 2\Omega) U_E &= \tau_n \\ \varepsilon \bar{u} \frac{\partial U_E}{\partial s} - (1 + \varepsilon \zeta) V_E &= \tau_s \end{split}$
Assumptions	Homogeneous deep ocean at rest.	Valid for plane parallel flows (e.g., straight jets); however, validity for curvilinear flows has been questioned by Wenegrat & Thomas.	Curvilinear flows, with Ekman Rossby number <<1 and the balanced Rossby number <1.

Numerical Simulations

Typically, wind stress is applied as a body force over the ocean upper layer. We instead assume a thin Ekman-like layer embedded in the upper layer. **Divergent Ekman transports** then enter into the upper layer mass equation. We compare different formulations using a two-layer shallow water model.

Simulations	Standard method	New method

Processes		Wind forcing → upper layer	Wind forcing \rightarrow modified Ekman layer \rightarrow upper layer
Equations	Ekman transport		$\frac{\partial}{\partial t}\vec{U}_E + (\vec{u}_1 \cdot \nabla)\vec{U}_E + (\vec{U}_E \cdot \nabla)\vec{u}_1 + f\hat{z} \times \vec{U}_E = \vec{\tau} - A_h \nabla^4 \vec{U}_E$
	Upper-layer momentum	$\frac{\partial}{\partial t}\vec{u}_1 + (\vec{u}_1 \cdot \nabla)\vec{u}_1 + f\hat{z} \times \vec{u}_1 = \frac{\vec{\tau}}{h_1} - A_h \nabla^4 \vec{u}_1$	$\frac{\partial}{\partial t}\vec{u}_1 + (\vec{u}_1 \cdot \nabla)\vec{u}_1 + f\hat{z} \times \vec{u}_1 = -A_h \nabla^4 \vec{u}_1$
	Upper-layer mass	$\frac{\partial}{\partial t}h_1 + \nabla \cdot (h_1 \vec{u}_1) = 0$	$\frac{\partial}{\partial t}h_1 + \nabla \cdot (h_1 \vec{u}_1) = -w_E$

Note that W&T formulation has been carried out in curvilinear coordinates, thus, it would be difficult to apply their Ekman equations to complicated background flow fields, e.g., jets with a random shape, turbulent eddies, etc.

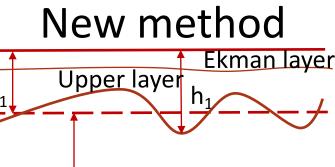
We extend the W&T Ekman formulation by adding a time-dependent term. This step removes the need for integrating over streamlines, and also introduces a near-inertial component to the Ekman pumping.

What factors impact the response of ocean interior flow to surface wind stress?

1. Representation of the Ekman layer 2. Interaction between eddies and the Ekman layer



Standard method Upper layer H₂ Lower layer



Lower layer

We also consider other simple formulations, e.g., using $\frac{\tau}{H_1}$ as a body force or the classic Ekman pumping as a forcing for the upper-layer mass equation. However, only the "standard" and "new" methods are considered here.

> Next, let's consider the upper-layer

Analysis: Steady Wind Stress with Shear

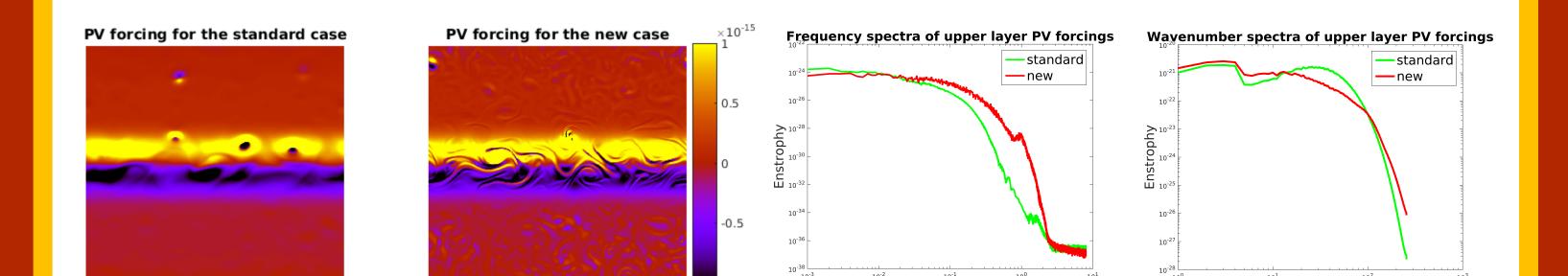


We introduce a time-dependent Ekman layer which interacts with eddy velocities. This new representation of the Ekman layer benefits associated dynamical processes.

First, let's look at the forcings. We focus on PV forcing to get an "apples-to-apples" comparison.

Here, we analyze the RHS of the upper-layer PV equations, which can be called PV forcings.

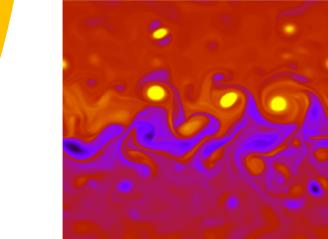
Simulations	Standard method	New method
Upper-layer PV equations	$\frac{Dq_1}{Dt} = \frac{1}{h_1} (\nabla \times \frac{\vec{\tau}}{h_1})$	$\frac{Dq_1}{Dt} = \frac{q_1}{h_1} w_E$

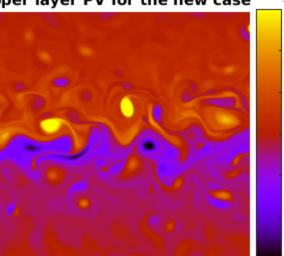


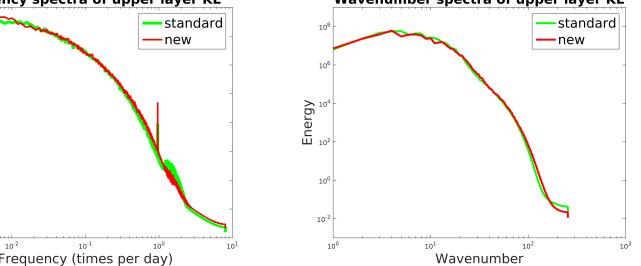


response

pper layer PV for the new case

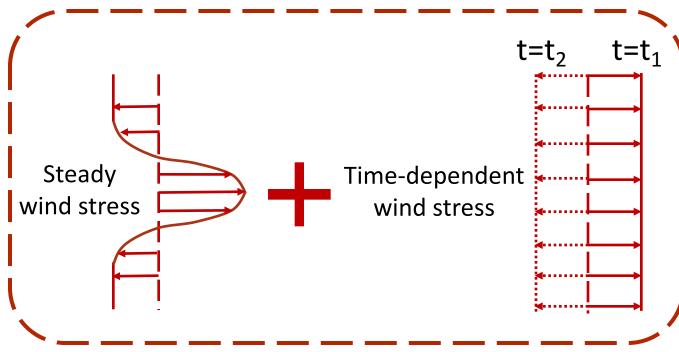






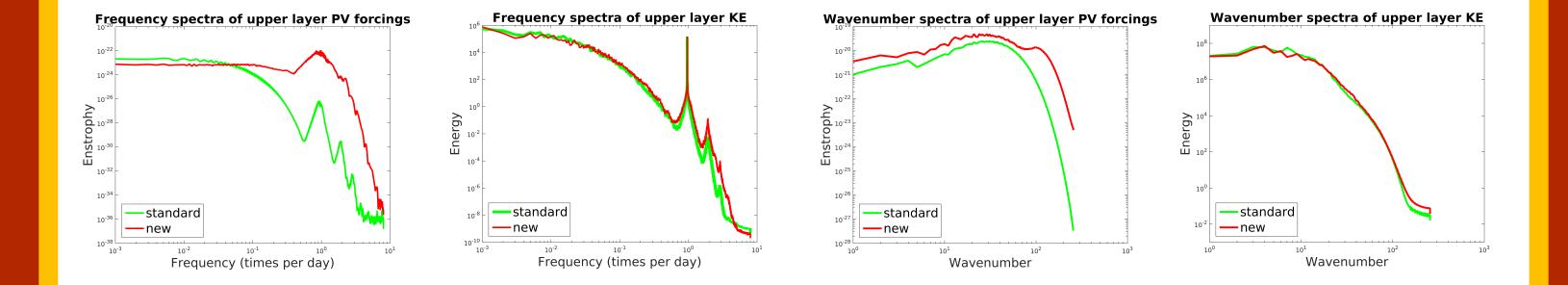
In contrast to notable differences in PV forcing, upper-layer kinetics of different simulations act similarly.

We next add a high-frequency component to the wind, which oscillates at Coriolis frequency. Again, large differences are evident in the (PV) forcing fields, but these do not lead to large differences in the response. Our future work asks why.



The new forcing shows more enstrophy input at high-frequencies, whereas the standard forcing shows a peak at intermediate-to-small scales. The latter appears related to coherent eddies with large interface height displacements.

Frequency (times per day



References

[1] Wenegrat and Thomas. Ekman transport in balanced currents with curvature. [2] Niiler. On the Ekman divergence in an oceanic jet.

[3] Stern. Interaction of a uniform wind stress with a geostrophic vortex.

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